## **Technical Notes**

TECHNICAL NOTES are short manuscripts describing new developments or important results of a preliminary nature. These Notes cannot exceed 6 manuscript pages and 3 figures; a page of text may be substituted for a figure and vice versa. After informal review by the editors, they may be published within a few months of the date of receipt. Style requirements are the same as for regular contributions (see inside back cover).

# **Upstream-Influence Scaling of Sharp Fin Interactions**

Frank K. Lu\*
University of Texas at Arlington
Arlington, Texas 76019
and
Gary S. Settles†
Pennsylvania State University
University Park, Pennsylvania 16802

#### Introduction

PSTREAM influence is a salient feature of all shockwave/boundary-layer interactions. For sharp-fin-generated swept interactions a scaling law has been developed<sup>1,2</sup> to describe the upstream influence as a function of Reynolds number and normal Mach number. Most of the data validating this fin-interaction scaling law,

$$\tilde{\xi}_U/M_n = f(\tilde{\xi}_U) \tag{1}$$

where  $\tilde{\xi}_U = (\xi_U/\delta)Re_\delta^b$ ,  $\tilde{\zeta}_U = (\zeta_U/\delta)Re_\delta^a$ , a=b=1/3 are empirical constants, and  $(\xi,\zeta)$  is a shock-based coordinate system (Fig. 1), were obtained at Mach 3 (Ref. 1). This Note presents data extending Eq. (1) to Mach numbers of 2.5-4. Furthermore, arguments are presented to suggest that this scaling law may be valid over a wider Mach number range by making a connection between Eq. (1) and classical hypersonic similarity.

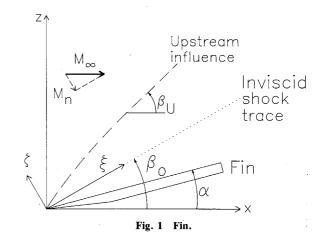
Fin interactions were studied at  $M_{\infty}=2.47, 2.95, 3.44$ , and 3.95 with corresponding Re=54, 59, 64, and  $76\times10^6$  m<sup>-1</sup>. The undisturbed boundary layer developing over the flat-plate test surface transitioned naturally and was two dimensional, turbulent, adiabatic, and in equilibrium at the test region. The incoming boundary-layer thickness  $\delta$  was 3.3  $\pm$ 0.1 mm for the four Mach numbers.<sup>2</sup>

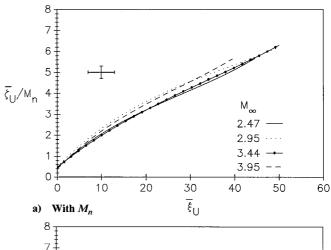
The upstream-influence data from surface-flow visualization ( $\xi_U$ ,  $\zeta_U$ ) were normalized by  $\delta$  (indicated by overbars on the symbols). At each of the four individual Mach numbers, the upstream influence scales according to

$$\bar{\zeta}_U/M_n = f(\bar{\xi}_U) \tag{2}$$

(plots not shown for brevity). To further determine if there is a residual  $M_{\infty}$  effect in the scaling, the scaled data at each Mach number were replaced by third-order least-squares curve fits to simplify the task of examining the 36 test cases. The

standard deviation of the data scatter about the fitted curve at each Mach number was  $\pm 5$ -10% and is indicated by a cross in Figs. 2a and 2b. The curve fits in Fig. 2a show that Eq. (2) is applicable to  $2.5 \le M_{\infty} \le 4.0$ , with no noticeable  $M_{\infty}$  effect within the data scatter. Thus, the effect of shock strength on the interaction scaling can be accounted for by a shock-based coordinate system and a scaling by  $M_n$ , as expected in a quasiconical interaction.<sup>1</sup>





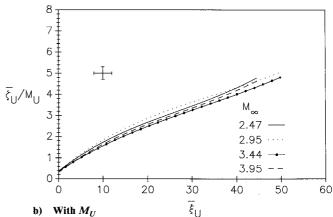


Fig. 2 Interaction scaling.

Received April 19, 1990; revision received July 9, 1990; accepted for publication July 24, 1990. Copyright © 1990 by the American Institute of Aeronautics and Astronautics, Inc. All rights reserved.

<sup>\*</sup>Assistant Professor, Aerospace Engineering Department, P.O. Box 19018. Member AIAA.

<sup>†</sup>Professor, Mechanical Engineering Department, and Director, Gas Dynamics Laboratory, M. E. Building. Associate Fellow AIAA.

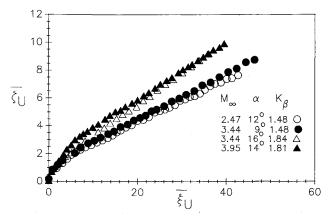


Fig. 3 Hypersonic similarity of the upstream-influence line.

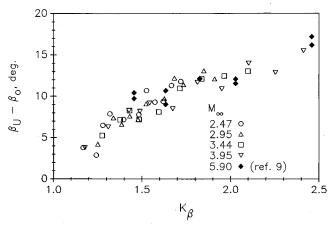


Fig. 4 Hypersonic similarity of  $(\beta_U - \beta_o)$ .

Furthermore, from the present data we infer that there is a negligible  $M_{\infty}$  effect on the Reynolds number scaling constants a and b. With the Reynolds number kept fairly constant for the four test Mach numbers, the data correlated well according to Eq. (1) with a = b = 1/3. Inger's analysis<sup>4</sup> showed that a and b also depend on the wake strength parameter of the incoming boundary layer. However, in the present experiments  $\Pi$  was essentially constant (0.54–0.58).

A quasiconical free-interaction principle also holds for fin interactions. <sup>5,6</sup> In particular, for separated interactions the upstream-influence line also marks the most upstream excursion of the unsteady separation shock. The upstream-influence line lies at an angle  $\beta_U$  (Fig. 1), and its inclination angle scales with  $M_U=M_\infty\sin\beta_U$  (Ref. 6). Therefore, the interaction may be expected to scale according to

$$\bar{\zeta}_U/M_U = f(\bar{\xi}_U) \tag{3}$$

Third-order least-squares curve fits to the data sets at each value of  $M_{\infty}$  are plotted in Fig. 2b, illustrating this behavior. This scaling, previously reported by Zheltovodov et al.,<sup>7</sup> reinforces the local similarity concept embodied in the quasiconical free-interaction principle.

Inviscid hypersonic flows past slender bodies of thickness-to-chord ratio  $\tau$  scale according to a hypersonic similarity parameter,  $K = M_{\infty} \tau$ .<sup>8</sup> Analogously, swept (hypersonic) interaction scaling by  $M_n$  or  $M_U$  is similar to scaling by  $K = M_{\infty} \alpha$  since  $M_n = M_{\infty} \sin \beta_o \approx M_{\infty} \beta_o = K_{\beta}$  and  $\lim_{M_{\infty} \to \infty} K_{\beta} \to K$ . In the supersonic regime, however,  $K_{\beta}$  appears to be a better similarity parameter. Two examples from the present experi-

ments with approximately equal values of  $K_{\beta}$  correlate well (Fig. 3), demonstrating this hypersonic similarity scaling by  $K_{\beta}$ . Furthermore, the far-field slope of  $\bar{\zeta}_U$ ,  $\tan^{-1}(\beta_U-\beta_o)$ , can be obtained. Figure 4 shows that  $(\beta_U-\beta_o)$  also scales with  $K_{\beta}$ . The figure includes data extracted from surface pressure measurements by Law, 9 who provide some additional evidence to the validity of the proposed hypersonic scaling. (Further work at high Mach numbers with larger values of  $K_{\beta}$  is necessary to properly demonstrate the validity of the proposed hypersonic scaling.)

The preceding evidence demonstrates that hypersonic similarity, although rooted in inviscid theory, is applicable to strong viscous-inviscid interactions as well. This reinforces a previously stated view<sup>1</sup> that inviscid parameters are dominant in the overall scaling of such interactions. Viscous effects are accounted for by  $Re_{\delta}^{1/3}$  in Eq. (1). Hence, the complete interaction scaling parameter  $Re_{\delta}^{1/3}/M_n$  is, in the hypersonic limit, simply  $Re_{\delta}^{1/3}/K$ .

As an afterthought, Korkegi's and Zheltovodov's incipient separation criteria, <sup>1</sup>

$$M_{\infty}\alpha_{\rm incip}=K_{\rm incip}=0.3$$
 and  $M_{\infty}\alpha_{\rm 2incip}=K_{\rm 2incip}=0.6$  (4)

respectively (where  $\alpha$  is in radians), can be viewed as results of hypersonic similarity. Incipient separation appears remarkably insensitive to Reynolds number in studies conducted to date. However, the dependence of the interaction on the incoming boundary-layer state (e.g., the wake parameter<sup>4</sup>) or on wall temperature conditions have not been thoroughly investigated.

### Acknowledgments

The data were obtained at Pennsylvania State University's Gas Dynamics Laboratory from experiments funded by AFOSR Grant 86-0082 monitored by L. Sakell and by NASA Ames Joint Research Interchange NCA2-192 with C. C. Horstman as the research collaborator. The authors thank the reviewer for suggesting that Law's data be examined for evidence of hypersonic similarity.

#### References

<sup>1</sup>Settles, G. S., and Dolling, D. S., "Swept Shock Wave/Boundary-Layer Interactions," *Tactical Missile Aerodynamics*, edited by M. J. Hemsch and J. N. Nielsen, Progress in Astronautics and Aeronautics, Vol. 104, AIAA, New York, 1986, pp. 297–379.

<sup>2</sup>Lu, F. K., Settles, G. S., and Horstman, C. C., "Mach Number Effects on Conical Surface Features of Swept Shock Boundary-Layer Interactions," *AIAA Journal*, Vol. 28, No. 1, 1990, pp. 91-97.

<sup>3</sup>Lu, F. K., and Settles, G. S., "Upstream-Influence Scaling of Fin-Generated Shock Wave Boundary-Layer Interactions," AIAA Paper 90-0376, Jan. 1990.

<sup>4</sup>Inger, G. R., "The Role of Law of the Wall/Wake Modeling in Validating Shock-Boundary Layer Interactions," AIAA Paper 88-3580, July 1988.

<sup>5</sup>Settles, G. S., and Kimmel, R. L., "Similarity of Quasiconical Shock Wave/Turbulent Boundary-Layer Interactions," *AIAA Journal*, Vol. 24, No. 1, 1986, pp. 47–53.

<sup>6</sup>Lu, F. K., and Settles, G. S., "Structure of Fin-Shock/Boundary Layer Interactions by Laser Light-Screen Visualization," AIAA Paper 88-3801, July 1988.

<sup>7</sup>Zheltovodov, A. A., Maksimov, A. I., and Shilein, E. K., "Development of Turbulent Separated Flows in the Vicinity of Swept Shock Waves," *The Interactions of Complex 3-D Flows*, edited by A. M., Kharitanov, Inst. of Theoretical and Applied Mechanics, Novosibirsk, USSR, 1987, pp. 67-91 (English translation).

<sup>8</sup>Anderson, J. D., Jr., *Hypersonic and High Temperature Gas Dynamics*, McGraw-Hill, New York, 1989, pp. 89–100.

<sup>9</sup>Law, C. H., "Three-Dimensional Shock Wave-Turbulent Boundary Layer Interactions at Mach 6," Air Force Aerospace Research Lab. Rept. ARL 75-0191, Wright-Patterson AFB, Ohio, 1975.